



Chemical Precipitation as Primary or Polishing Process for Phosphorus Removal

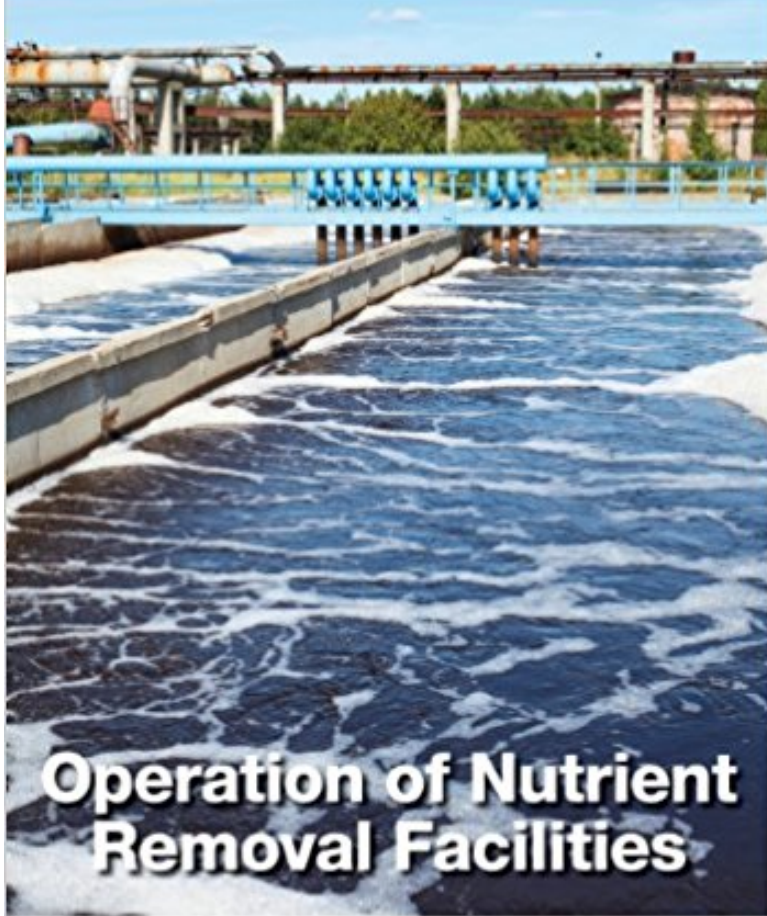
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Operation of Nutrient Removal Facilities

 **wef** Manual of Practice No. 37

Why Chemical P Removal?

- Often method of choice for small plants
- Retrofit to bio-P may be not practical
- Bio-P is subject to upsets – back-up
- Utilized as polishing step

Chemical addition is an integral part of any phosphorus removal facility either as a primary, polishing or back-up process



Overview

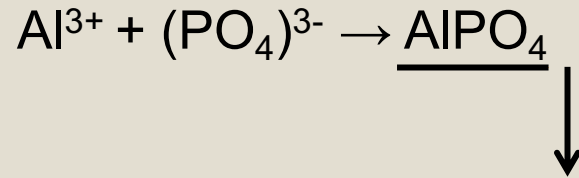
Chemical addition is an integral part of any phosphorus removal facility either as a primary, polishing or back-up process

1. Basics of chemical precipitation
2. Chemicals for P removal
3. Summary dose formulas
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5. Point of addition considerations
6. Response time and start-up
7. Sludge generation and inerts accumulation
8. Pros and Cons of chemical P removal

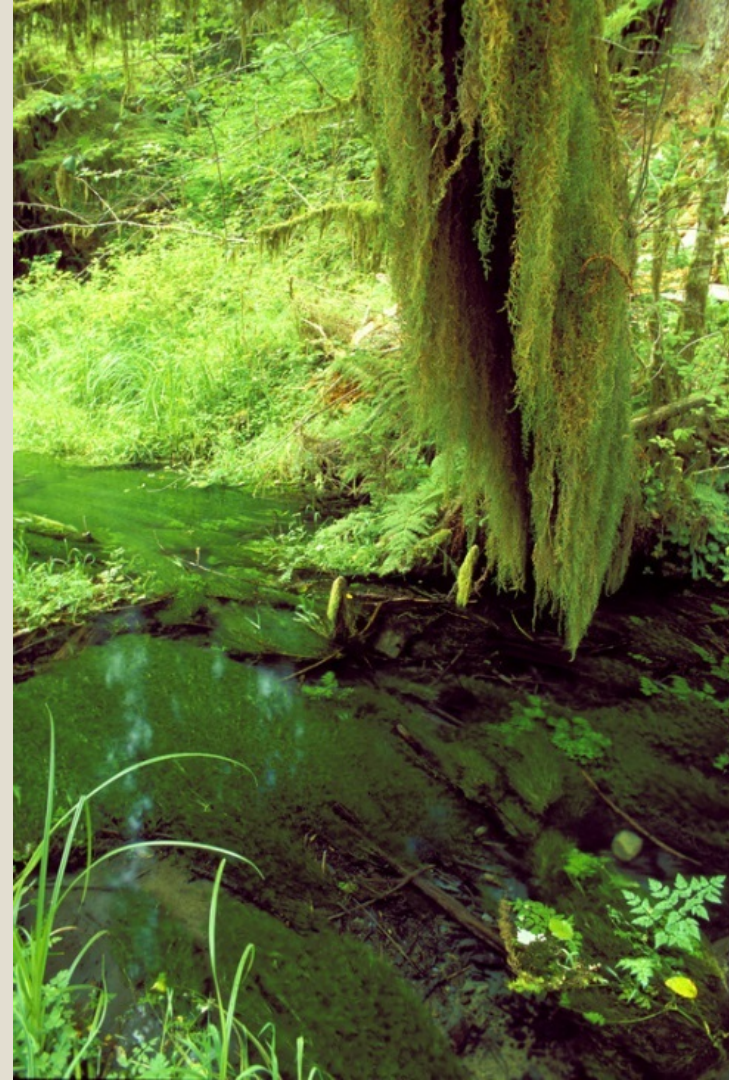
1 Basics

P present in different forms; soluble, colloidal and particulate

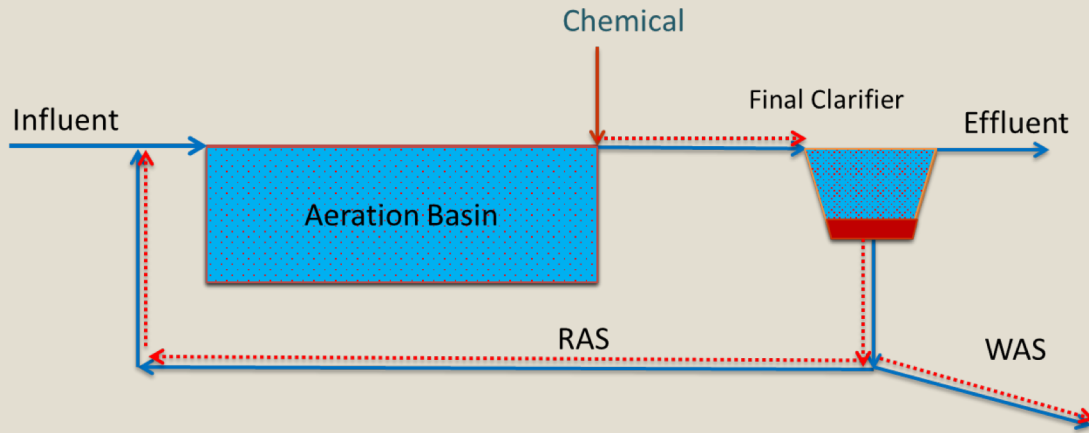
- orthophosphates (PO_4^{3-}) could be precipitated



- After biological treatment almost all residual P is in orthophosphate form
- Small concentration (<0.05 mg/L) of non-reactive, dissolved organic P may be present



1 Basics – Fate of Added Chemicals



- Chemical reacts with orthophosphate and precipitates as, say, aluminum orthophosphate
- Excess chemical also precipitates (aluminum hydroxide)
- Both forms settle and return with RAS to Aeration Basin

2 Chemicals for P Removal

- Aluminum-based chemicals
 - Alum (aluminum sulfate)
 - Polyaluminum chloride (PACl)
 - Sodium aluminate
- Iron-based compounds
 - Ferric chloride (FeCl_3) or sulfate
 - Ferrous salts (acidic spent pickle liquor)
- Other (lime, magnesium hydroxide)
- Water sludges
- Proprietary formulations



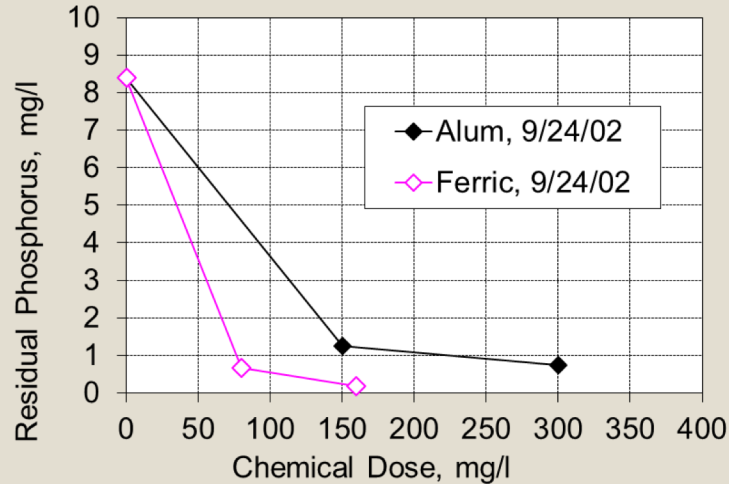
2 Chemicals - Selection

- Alternative chemicals are manufactured with, or contain, neutralizing agent (caustic)
- Could help with pH and be easier to handle
- Conduct side by side tests comparing effectiveness of alternative chemicals at various dosages and factor in unit costs



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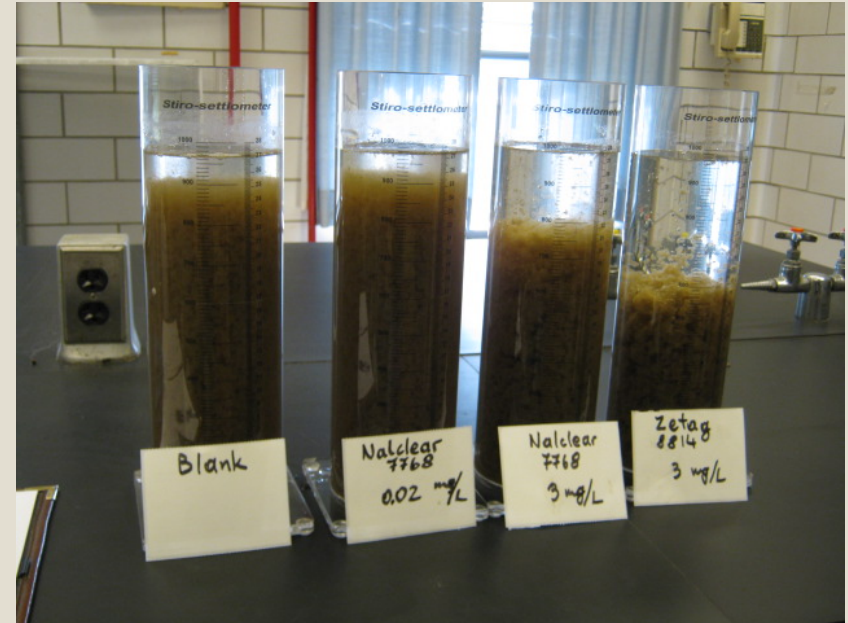
Chemical - Selection



- With application costs established, consider intangibles such as ease of handling, need for additional chemicals (caustic), help with odor, impact on UV

2 Chemical – Role of Polymer

- Not a P- precipitating agent on its own
- Could greatly improve settling
- Should be added downstream of precipitating chemicals
- 0.5 to 1 mg/L typical dose for dry polymer, higher for emulsion



3 Summary Dose Formula - Alum

Formula for calculating approximate alum dose for P removal is as follows (from MOP 37):

US Units

$$A = 11.8 * (X_i - X_e) * (Q / (1 - 0.95 * (\exp(-1.9 * X_e))))$$

- A = 49% alum solution application rate (gpd)
- X_i = soluble phosphorus concentration at the application point (mg/L)
- X_e = target effluent soluble phosphorus concentration (mg/L)
- Q = facility flow (mgd)

3 Summary Dose Formula - Ferric

US Units

$$A = 15.5 * (X_i - X_e) * (Q / (1 - 1.07 * (\exp(-2.25 * X_e))))$$

- A = 37% ferric chloride application rate (gpd)
- X_i = soluble phosphorus concentration at the application point (mg/L)
- X_e = target effluent soluble phosphorus concentration (mg/L)
- Q = facility flow (mgd)

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Formulas – Example (Ferric)

US Units

$$A = 15.5 * (X_i - X_e) * (Q / (1 - 1.07 * (\exp(-2.25 * X_e))))$$

- $X_i = 3 \text{ mg/L}$
- $X_e = 0.4 \text{ mg/L}$
- $Q = 10 \text{ mgd}$
- $A = 15.5 * (3 - 0.4) * (10 / (1 - 1.07 * \exp(-2.25 * 0.4)))$
- $A = 713 \text{ gpd of } 37\% \text{ ferric chloride}$

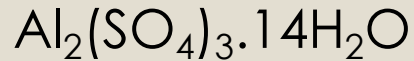
As 1 gallon of 37% ferric has 4.2 lb of FeCl_3 , the applied dose will be:

$$713 * 4.2 / 10 / 8.34 = 36 \text{ mg/L (as } \text{FeCl}_3\text{)}$$

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Formulas – Notes on Alum

Alum dose is customarily expressed as dry aluminum sulfate or “filter alum” with composition of:



49% Alum solution has dry alum ((Al₂(SO₄)₃*14H₂O) content of 0.647 kg/L (**5.4 lb/gal**), and aluminum metal content of 0.059 kg/L (0.492 lb/gal)



Dry alum, includes crystallization water!

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Formulas – Notes

- 37% Ferric chloride solution has specific density of 1.36 kg/L (11.4 lb/gal), dry FeCl_3 content of 0.504 kg/L (**4.2 lb/gal**) and iron metal content of 0.173 kg/L (1.44 lb/gal)
- Many factors (wastewater chemistry, pH, application point, mixing) will impact the actual dose
- Formulas are valid in a limited concentration range (for alum - 0.1 to 0.8 mg/L residual P)
- Multi-point addition of coagulant (e.g. some to primary clarifier, some to secondary clarifier) will result in reducing the overall chemical use

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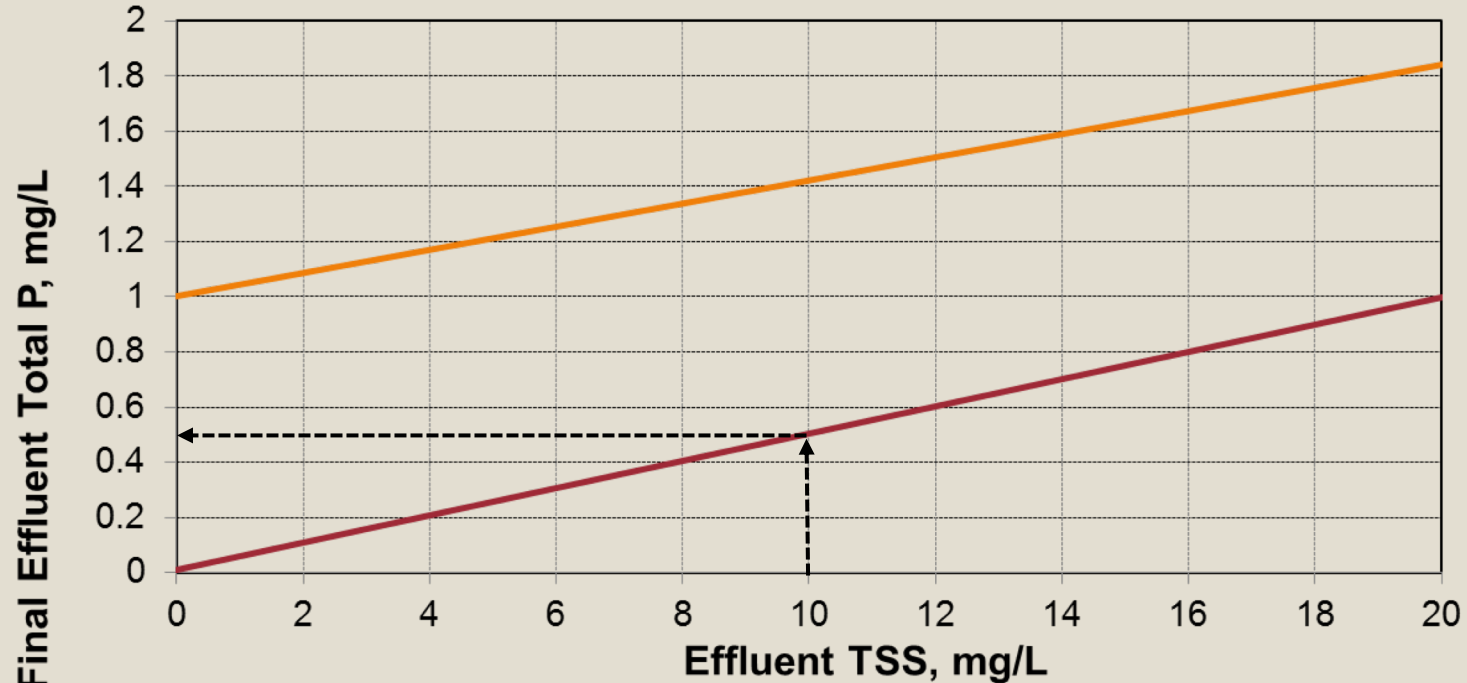
Role of Solids Separation

- P limits are commonly expressed as total P, so precipitating soluble P is only part of the job
- This is particularly important for low P limits
- MLSS (and effluent TSS) has approximately 2% of P; this could increase to 4-5% or even higher for plant removing P to a low level



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Role of Solids Separation – Impact of Effluent TSS on Effluent TP

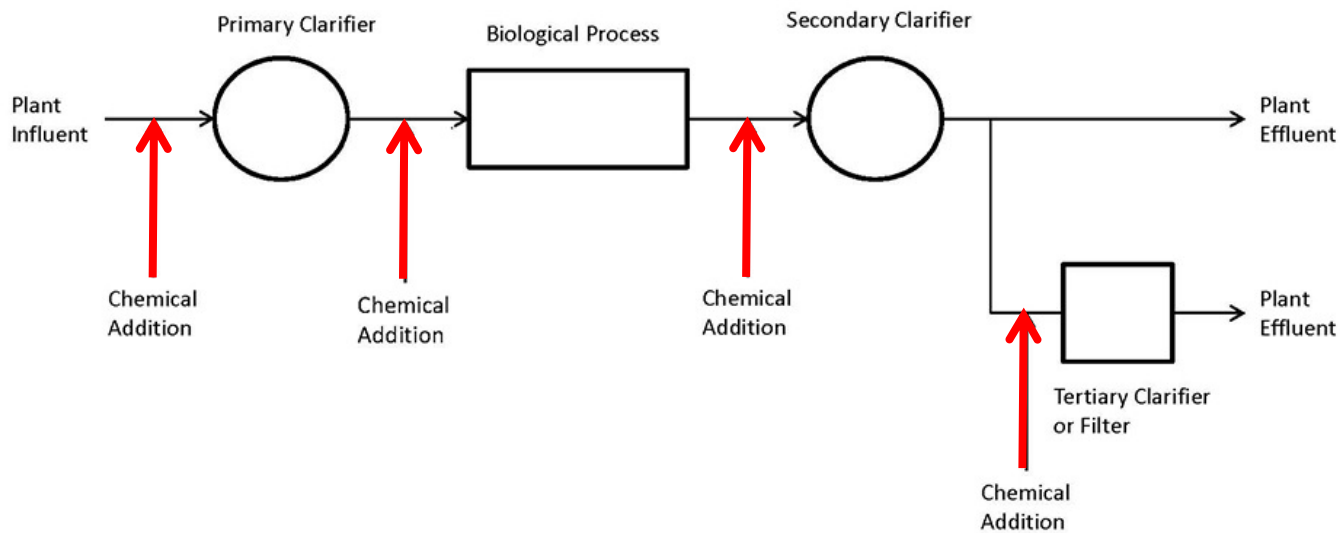


- Moderate P limit (effl. ortho-P = 1 mg/l), 0.042 mg P/mg TSS
- Low P limit (effl. ortho-P < 0.02 mg/l), 0.049 mg P/mg TSS

Primary effluent composition: tP = 5.25 mg/L, TSS = 84 mg/L, BOD5 = 142.5 mg/L. Alum added to activated sludge. Results obtained with BioWin modeling at SRT of 8 days

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Point of Addition Locations



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Point of Addition Considerations

- Point of addition should be upstream of the solids separation step (clarifier or filter)
- Vigorous mixing at the point of coagulant addition improves removal effectiveness
- If addition to filter or tertiary clarifier is possible, recycling sludge to primary clarifier will lower chemical use



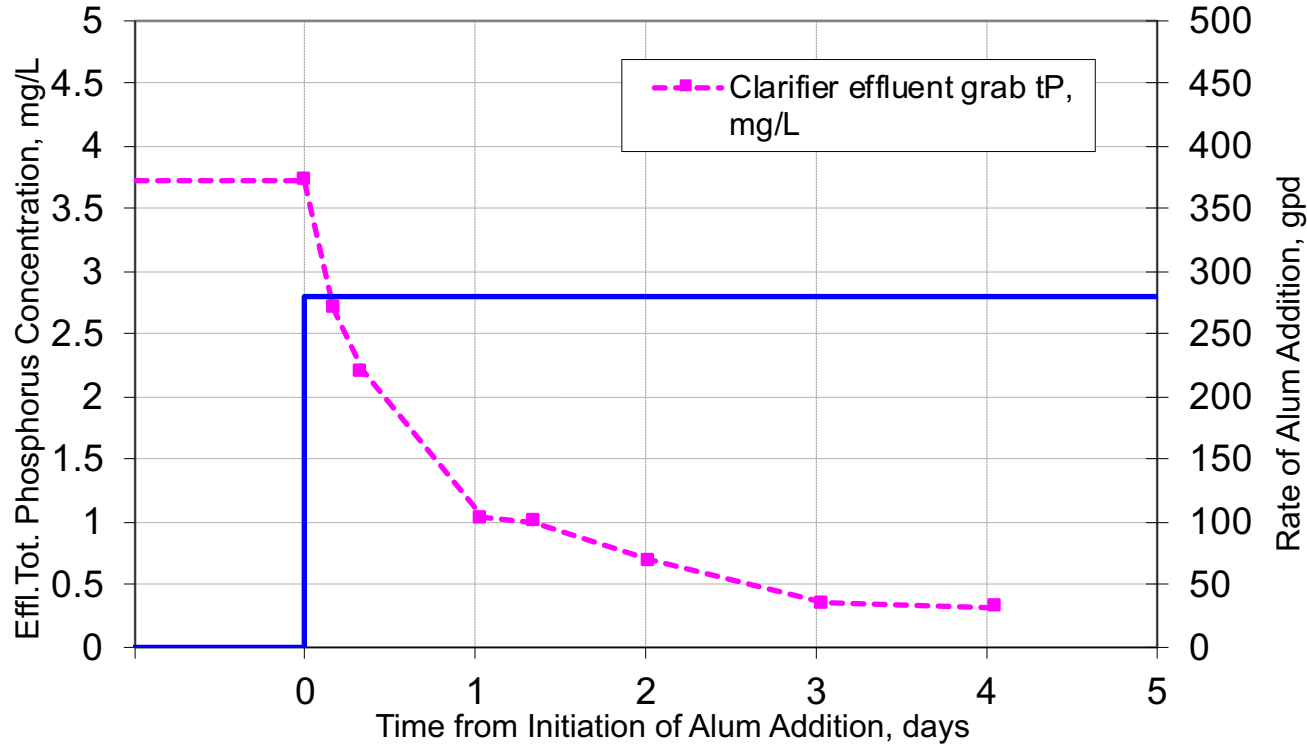
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Response Time and Start-Up

- Can be initiated on demand, with quick initial response
- When adding to activated sludge (final clarifier), full effects may take several days
 - Coagulation of biomass inventory
 - Unused chemical returned with RAS
 - HRT in any downstream processes

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Start-Up of Chemical Addition



7 Sludge Generation

- Chemical addition generates additional, inert sludge
- Chemical sludge is enmeshed with biomass and WAS (if added to activated sludge)
- Coagulants will increase capture of colloidal solids
- Approximate extra sludge generation can be calculated from conversion factors



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Sludge Generation (&TDS) Conversion Factors

Chemical/Process	TSS increase factor (F), kg per kg (or mg/L per mg/L) of chemical added	TDS increase factor, kg per kg (or mg/L per mg/L) of chemical added
Typical alum application for chemical P removal (at 3:1 alum to phosphorus stoichiometric rate), w/o neutralization	0.312	0.378
Typical alum application for chemical P removal (at 3:1 alum to phosphorus stoichiometric rate), with full neutralization with caustic	0.312	0.533
Typical ferric application for chemical P removal (at 3:1 ferric to phosphorus stoichiometric rate), w/o neutralization	0.748	0.460
Typical ferric application for chemical P removal (at 3:1 ferric to phosphorus stoichiometric rate), with full neutralization with caustic	0.748	0.745
pH adjustment with caustic	0	0.575
pH adjustment with sulfuric acid	0	0.980

7 Waste Sludge Generation - Example

- In our previous example, the 37% ferric application rate at a 10 mgd plant was 713 gpd or 36 mg/L
- From the Table, TSS conversion factor for Ferric (with 3:1 excess) was 0.748
- Thus extra sludge generated will be:

US Units

$$0.748 * 36 \text{ mg/L} = 27 \text{ mg/L extra TSS}$$

or,

$$713 \text{ gpd} * 4.2 \text{ lb FeCl}_3/\text{gal} = 2,995 \text{ lb FeCl}_3/\text{day}$$

$$0.748 * 2,995 \text{ lb FeCl}_3/\text{day} = 2,240 \text{ lb/d sludge}$$

7 Insert Sludge Accumulation in MLSS

- Inert, precipitated chemicals accumulate in aeration tankage, increasing non-volatile MLSS concentration
- Higher MLSS concentration required to maintain the same MLVSS (or sludge age)
- If the same MLSS is maintained, MLVSS concentration (and sludge age) will be lower (nitrification!)



7 Insert Sludge Accumulation in MLSS

$$MLSS_{ci} = D * F * SRT/HRT$$

- $MLSS_{ci}$ = chemical inerts concentration, mg/L
- D = chemical dose applied, mg/L
- F = TSS conversion factor for chemical used (from table)
- SRT = sludge age, days
- HRT = hydraulic retention time, days

7 Insert Sludge Accumulation - Example

- Flow = 10 mgd (37,850 m³/d)
- Tankage volume = 5 mg (18,925 m³)
- HRT = 0.5 day
- SRT = 12 days
- Ferric (37%) dose = 36 mg/L
- F = 0.748

$$\text{MLSSci} = 36 \text{ mg/L} * 0.748 * 12 \text{ d}/0.5 \text{ d} = 646 \text{ mg/L}$$

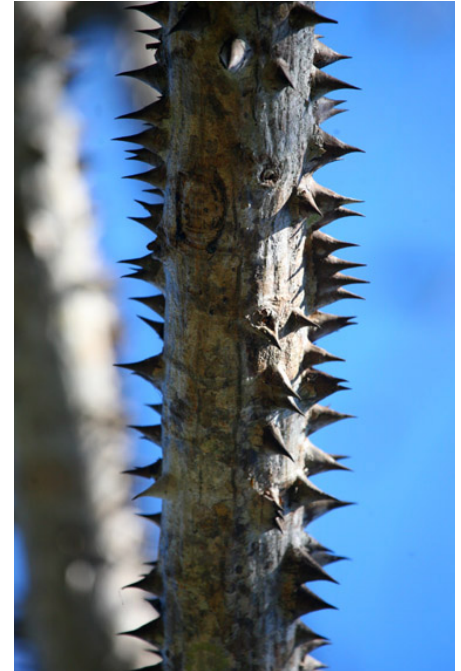
8 Summary – Pros and Cons

- Advantages:
 - Reliable
 - On demand
 - No issues with return streams P loading
 - Addition to primaries could help with lowering organic and N loadings to AS
 - Could help with odors (ferric)



8 Summary – Pros and Cons

- Disadvantages:
 - Operational costs of chemicals
 - Extra sludge disposal costs
 - Inert sludge impact on nitrification
 - Alkalinity consumption
 - TDS increase
 - Potential negative impact on UV (ferric)
 - Potential negative impact on WAS thickening (alum)
 - Overdosing could lead to P deficiency in downstream processes (denitrifying filter)



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Questions?

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